

## SE1CY15 Cybernetics and Circuits Feedback - Part C Prof Richard Mitchell

In the third quarter of the course the topics are

- Dynamic Feedback Systems
- Frequency Response
- Use of MatLab
- Introduction to time domain analysis

These will continue to be assessed by computer based labs

The topics build on last terms lectures

In this lecture we start by reminding us of these topics.

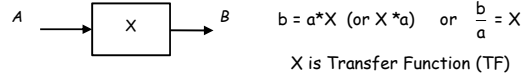
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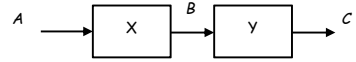


## 11 : Systems - a reminder

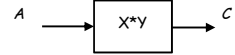
We analyse systems with inputs and outputs



Two blocks in series



Combine, for single TF



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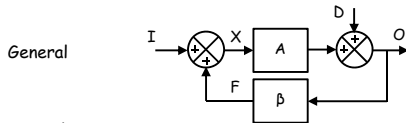
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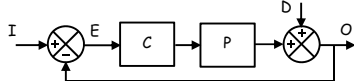
## Feedback Systems

We have considered two forms of feedback system

Have input I, output O, with disturbance D



Control System



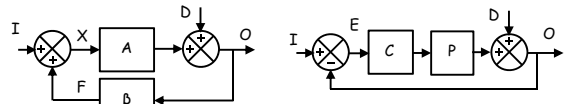
Analyse with 'forward over 1 minus loop' rule for overall TF

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## Using Forward over 1 minus Loop



Forward is TF input to O no loop; Loop is TF round loop

$$D = 0, \text{ Forward} = A \quad \frac{O}{I} = \frac{A}{1 - A\beta} \quad \text{Forward} = CP \quad \frac{O}{I} = \frac{C*P}{1 + C*P}$$

$$\text{Loop} = A\beta$$

$$I = 0, \text{ Forward, D..O} = 1 \quad \frac{O}{D} = \frac{1}{1 - A\beta} \quad \frac{O}{D} = \frac{1}{1 + C*P}$$

$$\text{Loop} = A\beta$$

Hence by Principle of Superposition  $O = \frac{A}{1 - A\beta} I + \frac{1}{1 - A\beta} D$   $O = \frac{C*P}{1 + C*P} I + \frac{1}{1 + C*P} D$

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## High Loop Gain

It is important for loop gain to be high (-ve or +ve)

$$O = \frac{A}{1 - A\beta} I + \frac{1}{1 - A\beta} D \quad O = \frac{C*P}{1 + C*P} * I + \frac{1}{1 + C*P} * D$$

$$A\beta \text{ big so } 1 - A\beta \sim -A\beta$$

$$CP \text{ big so } 1 + CP \sim CP$$

$$O \approx \frac{1}{-\beta} * I + 0 * D = -\frac{1}{\beta} * I$$

$$O \approx \frac{CP}{CP} * I + \frac{1}{CP} * D = I$$

O set by I and beta

largely unaffected if A changes.

largely unaffected by D.

O set by I

largely unaffected if P changes.

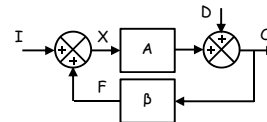
largely unaffected by D.

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## Lecture 11 In Class Exercise



Suppose

A = 990

beta = -0.1

- Find 1 minus Loop
- Find O/I assuming D = 0
- Find O/D assuming I = 0
- Evaluate O if I = 10 and D = -5
- Find O/I if A changed to 1000

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### Potential Divider

One of many electronic circuits that are feedback systems

$$V_o = \frac{R_2}{R_1 + R_2} V_s$$

$$I = \frac{V_s - V_o}{R_1}$$

And  $V_o = I * R_2$

Block Diagram Shows feedback!

So can model as

$$\frac{V_o}{V_s} = \text{Forward} = \frac{1}{1 - \text{Loop}} = \frac{\frac{1}{R_1} R_2}{1 - \frac{1}{R_1} R_2} = \frac{R_2}{R_2 + R_1}$$

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### Potential Divider with load:

Now  $V_o = R_2 * (I - I_L)$ , so

If  $I_L = 0$ ,  $\frac{V_o}{V_s} = \frac{\frac{1}{R_1} R_2}{1 - \frac{1}{R_1} R_2} = \frac{R_2}{R_2 + R_1}$

If  $V_s = 0$ ,  $\frac{V_o}{I_L} = \frac{-R_2}{1 - \frac{1}{R_1} R_2} = -\frac{R_1 R_2}{R_2 + R_1}$

By superposition:

$$V_o = \frac{R_2}{R_2 + R_1} V_s - \frac{R_1 R_2}{R_2 + R_1} I_L$$

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### Operational Amplifier

Also get feedback with operational amplifier (op amp) circuits

Two inputs and one output

$$V_o = A * (V_i^+ - V_i^-)$$

Model : summer + block with gain A

A very big,  $\sim 10^5$ , so if  $V_o$  say in range -10 to +10V

$$V_i^+ - V_i^- = V_o/A \sim 0: \text{ so } V_i^+ = V_i^-$$

To achieve this, we put feedback round them .. Such as

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### Operational Amplifier + Pot Divider

$V_i^-$  set by potential divider  
But  $V_i^- = V_i$  approximately:

$$\text{So } V_i^- = V_o \frac{R_2}{R_1 + R_2} \text{ or } \frac{V_o}{V_i^-} = \frac{R_1 + R_2}{R_2}$$

Block Diagram for complete analysis

$$\frac{V_o}{V_i} = \frac{A}{1 - A \frac{R_2}{R_1 + R_2}} \approx \frac{A}{A \frac{R_2}{R_1 + R_2}} = \frac{R_1 + R_2}{R_2}$$

<http://www.reading.ac.uk/~shsmchl/r/javascript/transfunc.html>

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### Put Some Values In

Suppose  $R_1 = 9 \text{ k}\Omega$  and  $R_2 = 1 \text{ k}\Omega$   
By approximate analysis

$$\text{So } \frac{V_o}{V_i} = \frac{1\text{k}}{9\text{k} + 1\text{k}} \text{ or } \frac{V_o}{V_i} = \frac{10\text{k}}{1\text{k}} = 10$$

For full analysis, assuming A is  $10^5$

$$\frac{V_o}{V_i} = \frac{10^5}{1 - 10^5 \frac{1\text{k}}{9\text{k} + 1\text{k}}} = \frac{10^5}{1 + 10^5 \frac{1}{10}} = \frac{10^5}{1 + 10000} = 9.999 \approx 10$$

Is A $\beta$  system:  $\beta = -0.1 : O/I \sim -1/\beta = 10 : |1 - A\beta| = 10001 > 1$

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### Blocks which Integrate

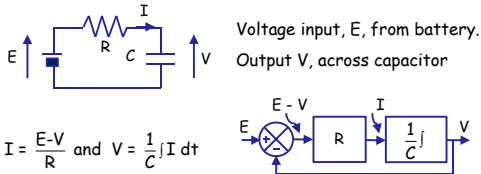
When we model a resistor, we use  $V = I * R$  or  $I = V/R$   
Output is a constant proportional to input

But, when I flows into a capacitor, the voltage V across it rises  
 $V = V + \text{amount due to I}$

$$V = 1/C * \text{Integral I}$$

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## RC Circuit



$$I = \frac{E-V}{R} \text{ and } V = \frac{1}{C} \int I dt$$

If  $V = 0$  initially, it will then rise as  $I$  flows.  
 When will it stop rising? When input to integrator is 0.  
 That is when  $I = 0$ , which is when  $E-V = 0$  or  $V = E$   
 This is its STEADY STATE value

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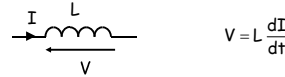


## Differentiator

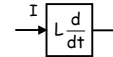
We note that a capacitor is modelled by an integrator

$$V = 1/C * \text{Integral } I$$

Another electronic component is an inductor



So a block diagram is



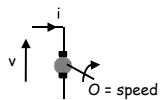
Point to note, we may need to integrate or to differentiate.

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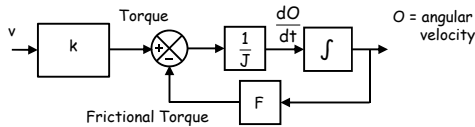
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## Also need Integrators for Motors



Voltage applied - means current flows  
 Generates torque making motor turn  
 Frictional torque opposes motion  
 Net Torque =  $MoI * \text{angular acceleration}$   
 Integrate this to get angular velocity

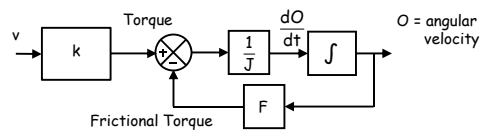


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## For Motor



For steady state:

$$\frac{dO}{dt} = 0 \text{ means } v*k - F*O = 0$$

$$\text{Hence } O = \frac{v*k}{F}$$

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## Two Key Questions

We have found the steady state value of the output  
 $V$  is steady state when  $V = \text{the constant } E$   
 Speed  $O$  is steady state when  $O = v*k/F$  constants  
 This is true if the system input ( $E$  or  $v$ ) is constant (after  $t=0$ )  
 What if it isn't?  
 Also ... if  $O = 0$  at time 0,  
 How does  $O$  get to its steady value?

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## Summary

In this lecture have reminded ourselves of  
 Block Diagrams      Feedback Systems : Forward / 1 - Loop  
 Importance of High Loop Gain  
 We have also looked at electronic circuits with feedback  
 The potential divider and op-amps  
 We have also considered blocks with integrators / differentiators  
 We can work out steady values for constant inputs  
 And posed two questions  
 Next week we address the first .. Assuming inputs are sinusoids  
 And start using complex numbers which actually make it easier ...

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### 12: Sinusoids and Feedback

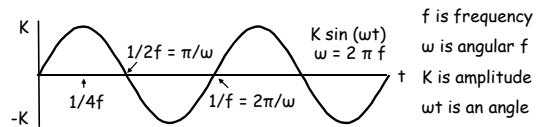
Last week we reminded ourselves about feedback systems  
 And looked at some electronic and motor systems  
 We model these by simple blocks we combine  
 Some blocks have the form output = input \* value  
 But some are integrators or differentiators.  
 We worked out the **steady state** output if the input is a **step**  
 In this lecture we analyse systems where the input is a **sinusoid**  
 Now we will see how blocks can process sinusoids  
 And model integration/differentiation using  $\sqrt{-1} = j$   
 We will introduce in context of electronics, but applies elsewhere

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### When Signals are Sinusoids



Note that cos is a shifted sin :  $\pm \cos(\omega t) = \sin(\omega t \pm \frac{\pi}{2})$

Also  $p \sin(\omega t) + q \cos(\omega t) = \sqrt{p^2 + q^2} \sin(\omega t + \tan^{-1} \frac{q}{p})$

The angle a in  $\sin(\omega t + a)$  is termed a phase shift

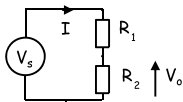
If one signal in system is a sinusoid, all others are sinusoids of **same** angular frequency with different **amplitudes** + may be **phase shifted**  
 Applies to all linear systems - found easily using complex numbers

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### Consider Pure Resistive System



Suppose  $R_1 = 1 \text{ k}\Omega$  and  $R_2 = 9 \text{ k}\Omega$   
 Also, suppose  $V_s = 5 \sin(7t)$

$$V_o = \frac{R_2}{R_1 + R_2} V_s = \frac{9}{10} 5 \sin(7t) = 4.5 \sin(7t)$$

$$I = \frac{V_s}{R_1 + R_2} = \frac{5 \sin(7t)}{10k} = 0.0005 \sin(7t)$$

All 3 signals, same frequency, different amplitude, no phase shift

<http://www.reading.ac.uk/~shsmchl/r/javascript/SinAndRC.html>

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### Sinusoidal Currents into R and/or C



$I = \sin(40t)$   
 $V = 5 \sin(40t)$

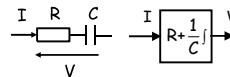


$$V = \frac{1}{0.01} \int \sin(40t) dt$$

$$= -\frac{1}{0.01 * 40} \cos(40t)$$

$$= -2.5 \cos(40t)$$

$$= 2.5 \sin(40t - \frac{\pi}{2})$$



$$V = 5 \sin(40t) - 2.5 \cos(40t)$$

$$= \sqrt{5^2 + 2.5^2} \sin(40t + \tan^{-1}(-\frac{2.5}{5}))$$

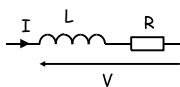
$$= 5.59 \sin(40t - 0.464)$$

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### In Class Exercise



Suppose  $I = \sin(40t)$ ,  $L = 0.2H$  and  $R = 6\Omega$

Find  $V = I R + L \frac{dI}{dt}$  as phase shifted sin

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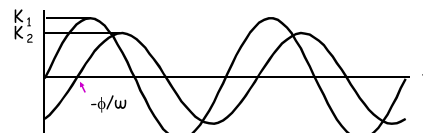


### These illustrate a Key General Point

For **any** linear system, **under steady state conditions**,

If input is  $K_1 \sin(\omega t)$ , output is  $K_2 \sin(\omega t + \phi)$

Sinusoid, same ang freq, diff amplitude and phase shifted



For block diagram analysis, need blocks which can **both** change **amplitude** and do a **phase shift** (ie angle shift) ...

We need numbers which have size and angle ...

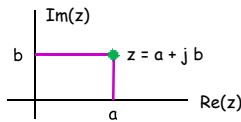
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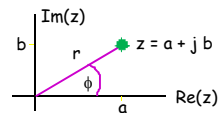


## Complex Numbers Give Size and Angle

$z = a + j * b$   $a$  is real part;  $b$  is imaginary part;  $j = \sqrt{-1}$



Plot on 2D graph, the Argand plane



Same point also defined by distance from 0,0 and angle from real axis

Distance  $r$  is modulus

Angle  $\phi$  is argument

$$|z| = r = \sqrt{a^2 + b^2}$$

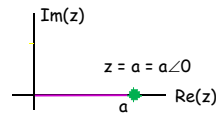
$$\angle z = \phi = \tan^{-1}\left(\frac{b}{a}\right)$$

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## Two Points to Note



A 'normal' number is a special case of a complex number

A point on 'real' axis

Value = distance from 0, angle 0

For systems often have  $z = \frac{z_1}{z_2}$

modulus and argument easy:  $|z| = \frac{|z_1|}{|z_2|}$  and  $\angle z = \angle z_1 - \angle z_2$

$$z = \frac{a + j b}{c + j d} \quad |z| = \frac{\sqrt{a^2 + b^2}}{\sqrt{c^2 + d^2}} \quad \angle z = \tan^{-1}\left(\frac{b}{a}\right) - \tan^{-1}\left(\frac{d}{c}\right)$$

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## Integration and Complex Numbers

Consider  $\frac{1}{j\omega}$ :  $\left| \frac{1}{j\omega} \right| = \frac{\sqrt{1^2 + 0^2}}{\sqrt{0^2 + \omega^2}} = \frac{1}{\omega}$   
 $\angle \frac{1}{j\omega} = \tan^{-1}\left(\frac{0}{1}\right) - \tan^{-1}\left(\frac{1}{0}\right) = -\tan^{-1}(\infty) = -\frac{\pi}{2}$

Has size  $\frac{1}{\omega}$  and angle  $-\frac{\pi}{2}$

But  $\int \sin(\omega t) = -\frac{1}{\omega} \cos(\omega t) = \frac{1}{\omega} \sin(\omega t - \frac{\pi}{2})$

Change of size by  $\frac{1}{\omega}$  and change angle by  $-\frac{\pi}{2}$

So  $\frac{1}{j\omega} \equiv \int$  Similarly,  $j\omega \equiv \frac{d}{dt}$

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## So Model for Capacitor and Inductor

Capacitor:  $I \rightarrow \left[ \frac{1}{C} \int \right] \rightarrow V$   $V = \frac{1}{C} \int I dt$  model by  $V = I * \frac{1}{j\omega C}$

Consistent with complex impedance  $Z = \frac{1}{j\omega C}$

Inductor:  $I \rightarrow \left[ L \frac{d}{dt} \right] \rightarrow V$  Inductor:  $V = L \frac{dI}{dt} = \omega L \cos(\omega t) = \omega L \sin(\omega t + \frac{\pi}{2})$

Model by  $j\omega L = \omega L \angle \frac{\pi}{2}$   $Z = j\omega L$

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## Hence for Block Diagrams

Resistor:  $I \rightarrow \left[ R \right] \rightarrow V$  or  $V \rightarrow \left[ \frac{1}{R} \right] \rightarrow I$

Capacitor:  $I \rightarrow \left[ \frac{1}{j\omega C} \right] \rightarrow V$  Inductor:  $I \rightarrow \left[ j\omega L \right] \rightarrow V$

And then

For any System, where  $I = \sin(\omega t)$ , we model it by a complex transfer function,  $H(j\omega)$ , and readily determine  $O \dots$

$I \rightarrow \left[ H(j\omega) \right] \rightarrow O$   $O = |H(j\omega)| \sin(\omega t + \angle H(j\omega))$

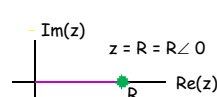
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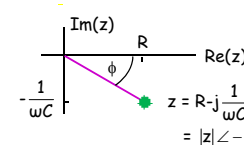


## Argand Plot for R, C and R + C

If  $I$  is  $\sin(\omega t)$ , find  $V$  across component(s)



$V = R \sin(\omega t)$



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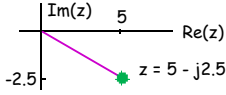


$z = R - j \frac{1}{\omega C} = \frac{1}{j\omega C} = \frac{1}{\omega C} \angle -\frac{\pi}{2}$   
 $V = \frac{1}{\omega C} \sin(\omega t - \frac{\pi}{2})$

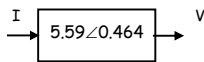
$V = |z| \sin(\omega t + \phi)$   
 $= \frac{1}{\sqrt{R^2 + (\frac{1}{\omega C})^2}} \sin(\omega t - \tan^{-1} \frac{1}{\omega CR})$

## With Some Values

Earlier example,  $I = \sin(40t)$ ,  $R = 5\Omega$ ,  $C = 0.01F$ ,  $1/\omega C = 2.5$



$$z = 5 - j2.5 = \sqrt{5^2 + 2.5^2} \angle \tan^{-1} \frac{-2.5}{5} = 5.59 \angle -0.464$$



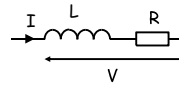
So  $V = 5.59 \sin(40t - 0.464)$

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## In Lecture Exercise



$I = \sin(40t)$ ,  $L = 0.2H$  and  $R = 6\Omega$

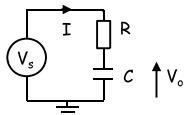
Do Argand plot for this find complex transfer functions and hence determine V

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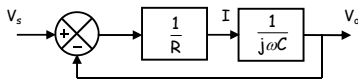
## Transfer Function for RC Circuit



Z for resistor = R; for capacitor =  $\frac{1}{j\omega C}$

Pot Divider  $\frac{V_0}{V_s} = \frac{\frac{1}{j\omega C}}{R + \frac{1}{j\omega C}} = \frac{1}{j\omega CR + 1}$

Or using block diagrams



$$\text{So } \frac{V_0}{V_s} = \frac{\text{Forward}}{1 - \text{Loop}} = \frac{\frac{1}{R} \cdot \frac{1}{j\omega C}}{1 - \frac{1}{R} \cdot \frac{1}{j\omega C}} = \frac{1}{j\omega CR + 1}$$

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## And So

$$\frac{V_0}{V_s} = \frac{1}{1 + j\omega CR} \quad \left| \frac{1}{1 + j\omega CR} \right| = \frac{1}{\sqrt{1 + \omega^2 C^2 R^2}} \quad \angle \frac{1}{1 + j\omega CR} = 0 - \tan^{-1} \omega CR$$

Suppose  $R = 1k\Omega$ ,  $C = 400 \mu F$  and  $V_s = 5 \sin(7t)$

$$\frac{V_0}{V_s} = \frac{1}{1 + j7 \cdot 400 \cdot 10^{-6} \cdot 1 \cdot 10^3} = \frac{1}{1 + j28 \cdot 10^{-2-6+3}} = \frac{1}{1 + j2.8}$$

$$\left| \frac{1}{1 + j2.8} \right| = \frac{1}{\sqrt{1 + 7.84}} = 0.336 \quad \angle \frac{1}{1 + j2.8} = -\tan^{-1} 2.8 = -1.23 \text{ rad}$$

Hence  $V_0 = 5 \cdot 0.336 \sin(7t - 1.23) = 1.68 \sin(7t - 1.23)$

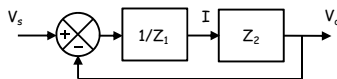
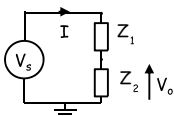
<http://www.reading.ac.uk/~shsmchl/r/javascript/SinAndRC.html>

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## In terms of General Impedances



$$\text{So } \frac{V_0}{V_s} = \frac{\text{Forward}}{1 - \text{Loop}} = \frac{\frac{1}{Z_1} \cdot Z_2}{1 - \frac{1}{Z_1} \cdot Z_2} = \frac{Z_2}{Z_2 + Z_1}$$

e.g If  $V_s = 10\sin(3t)$ ,  $Z_1 = j\omega 2 = j6$  and  $Z_2 = 8$

$$\frac{V_0}{V_s} = \frac{8}{8 + j6} = \frac{8}{\sqrt{64 + 36}} \angle -\tan^{-1} \frac{6}{8} = 0.8 \angle -0.644$$

Hence  $V_0 = 10 \cdot 0.8 \sin(3t - 0.644) = 8 \sin(3t - 0.644)$

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## Summary

In this lecture : systems where its signals are sinusoids

All same frequency

May have different amplitude - may be phase shifted

Amplitude and Phase shift found using complex numbers

**Key point - use complex numbers to model calculus**

We process by finding their modulus and argument

Shown working on electronics

Next week we develop this further,

looking at other systems, with the same form of model

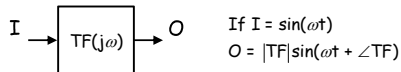
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## 13 : Modelling Other Systems

Last week we saw how to model circuits  
Including, as signals were sinusoids, how to represent integrators  
Hence using complex numbers



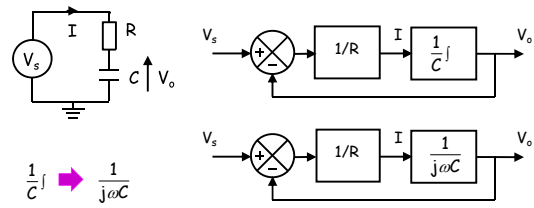
This week we develop this further and show  
that the concept applies to other (non electronic) systems  
First a reminder of the RC circuit from last week

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## RC Circuit Example



$$\text{So } \frac{V_o}{V_s} = \frac{\text{Forward}}{1 - \text{Loop}} = \frac{\frac{1}{R} \cdot \frac{1}{j\omega C}}{1 - \frac{1}{R} \cdot \frac{1}{j\omega C}} = \frac{1}{j\omega CR + 1}$$

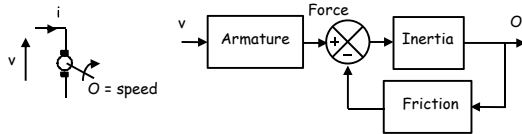
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## Motor

These concepts are not just applicable to electronics



v applied to armature circuit

- current i
- force to make motor move
- motor moves, output velocity O
- friction (which depends on velocity) opposes motion

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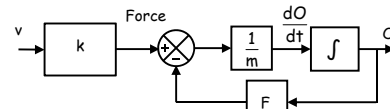
## Incorporating the Inertia

Net Force = that due to Current (= v\*k) - that due to Friction (F \* O)

Net Force = mass \* acceleration (Newton's 2<sup>nd</sup> Law)

Acceleration is change in (differential of), velocity

We want velocity, so we integrate acceleration for O



As  $v*k - F * O = \text{mass} * \text{acceleration}$

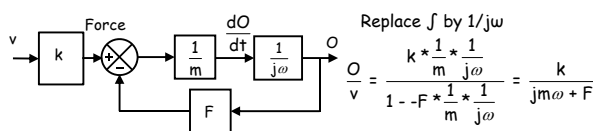
$$\text{acceleration} = \frac{dO}{dt} = \frac{\text{net force}}{\text{mass}} = \frac{v*k - F*O}{m}$$

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## Forward over 1 minus Loop



Replace ∫ by 1/jω

$$\frac{O}{v} = \frac{k * \frac{1}{m} * \frac{1}{j\omega}}{1 - F * \frac{1}{m} * \frac{1}{j\omega}} = \frac{k}{jm\omega + F}$$

So, if v is  $4 \sin(9t)$ ,  $k = 1 \text{ N/v}$ ,  $m = 0.2 \text{ kg}$ ,  $F = 0.1 \text{ N/m}$  (note units)

$$\frac{O}{v} = \frac{1}{j0.2*9 + 0.1} = \frac{1}{j1.8 + 0.1}$$

$$\left| \frac{1}{j1.8 + 0.1} \right| = \frac{1}{\sqrt{1.8^2 + 0.1^2}} = 0.55 \quad \angle \frac{1}{j1.8 + 0.1} = -\tan^{-1} \frac{1.8}{0.1} = -1.52$$

$$\text{So, } O = 2.2 \sin(9t - 1.52)$$

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## Rotational Movement

In the above example, the motor moves in straight line

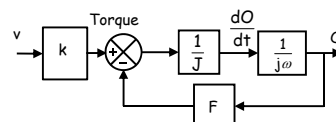
Its position (units m) changes, it moves with a given velocity (m/s)

It has mass (kg), it accelerates ( $\text{ms}^{-2}$ ), due to force (N)

If the motor rotates, its angular position (units rad) changes

Have angular velocity (rad/s), angular acceleration ( $\text{rad s}^{-2}$ ),

Due to torque (Nm), mass has moment of inertia J ( $\text{kgm}^2$ )



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**So**

$$\frac{O}{v} = \frac{k \cdot \frac{1}{J} \cdot \frac{1}{j\omega}}{1 - F \cdot \frac{1}{J} \cdot \frac{1}{j\omega}} = \frac{k}{jJ\omega + F}$$

So, if I is 4 sin(9t), k = 1 Nm/v, J = 0.2 kg m<sup>2</sup>, F = 0.1 Nm per rad/s

$$\frac{O}{v} = \frac{1}{j0.2 \cdot 9 + 0.1} = \frac{1}{j1.8 + 0.1}$$

$$\left| \frac{1}{j1.8 + 0.1} \right| = \frac{1}{\sqrt{1.8^2 + 0.1^2}} = 0.55 \quad \angle \frac{1}{j1.8 + 0.1} = -\tan^{-1} \frac{1.8}{0.1} = -1.52$$

So, O = 2.2 sin(9t - 1.52)

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**Permanent Magnet Motor**

v applied to armature circuit: motor turns e<sub>b</sub> 'back emf' generated  
 Difference between v and e<sub>b</sub> → V across R → current, i  
 i → torque T (= K\*i) → angular velocity O (note inertia/friction)  
 O → e<sub>b</sub> (= B\*O)  
 Slightly more complicated model ..

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**Full Block Diagram**

Use Forward over 1 - Loops

$$\frac{O}{v} = \frac{\frac{1}{R} \cdot K \cdot \frac{1}{J} \cdot \frac{1}{j\omega}}{1 - B \cdot \frac{1}{R} \cdot K \cdot \frac{1}{J} \cdot \frac{1}{j\omega} - F \cdot \frac{1}{J} \cdot \frac{1}{j\omega}}$$

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**Simplify**

$$\frac{O}{v} = \frac{\frac{1}{R} \cdot K \cdot \frac{1}{J} \cdot \frac{1}{j\omega}}{1 - B \cdot \frac{1}{R} \cdot K \cdot \frac{1}{J} \cdot \frac{1}{j\omega} - F \cdot \frac{1}{J} \cdot \frac{1}{j\omega}}$$

$$\frac{O}{v} = \frac{\frac{K}{j\omega R J}}{1 + \frac{BK}{j\omega R J} + \frac{F}{j\omega J}} \quad \text{Multiply by } \frac{j\omega R J}{j\omega R J}$$

$$\frac{O}{v} = \frac{K}{j\omega R J + BK + FR}$$

This is in same form as in previous examples  $\frac{O}{v} = \frac{K}{a + j\omega b}$

So if have values for K, R, J, B and know v, can work out O

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**Lecture 13 In Class Exercise**

For motor  $\frac{O}{v} = \frac{K}{j\omega R J + BK + FR}$

Suppose K = 0.1, R = 1k, J = 0.05, F = 0.01, B = 0.1 and v = 10sin(0.1t)  
 What is O?

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**Mechanical Example**

Force f applied to spring attached to wall  
 'Dashpot' represents friction opposing motion

When spring compressed by x, force k\*x opposes (Hooke's Law)  
 Frictional force = F \* differential of x also opposes

As  $\dot{x} \equiv \frac{1}{j\omega}$ , So  $\frac{d}{dt} \equiv j\omega$ . Hence dashpot force is F\*jω\*x

Hence f = k\*x + F\*jω\*x = (k + jωF) x

Hence  $\frac{x}{f} = \frac{1}{k + j\omega F}$

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**Standard Model**

For RC circuit First motor Perm. magnet motor Spring Sys

$$\frac{V_o}{V_s} = \frac{1}{1 + j\omega CR} \quad \frac{O}{I} = \frac{1}{jm\omega + F} \quad \frac{O}{v} = \frac{K}{j\omega RJ + BK + FR} \quad \frac{x}{f} = \frac{1}{k + j\omega F}$$

For convenience, it is useful to have a standard model  $\frac{K}{1+j\omega T}$

For RC circuit, already there : K = 1 and T = RC

For first motor For perm. magnet motor For Spring Sys

$$\frac{O}{I} = \frac{1}{jm\omega + F} = \frac{1/F}{1 + jm\omega/F}$$

$$\frac{O}{v} = \frac{K}{1 + j\omega \frac{BK + FR}{BK + FR}} = \frac{K}{1 + j\omega \frac{R}{BK + FR}}$$

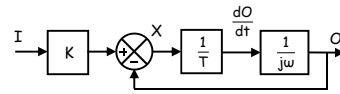
$$\frac{x}{f} = \frac{1}{1 + j\omega \frac{F}{k}}$$

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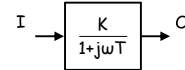
**Block Diagram For This Form**



Using Forward over 1-loop

$$\frac{O}{I} = \frac{K * \frac{1}{T} * \frac{1}{j\omega}}{1 - \frac{1}{T} * \frac{1}{j\omega}} = \frac{K}{1 + \frac{1}{j\omega T}} = \frac{K}{1 + j\omega T}$$

So System reduces to



<http://www.reading.ac.uk/~shsmchr/javascript/SysAndSin.html>

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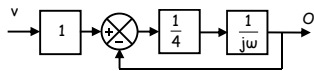


**Permanent Magnet Motor in this form**

$$\frac{O}{v} = \frac{K}{j\omega RJ + BK + FR}$$

Let K = 0.1, B = 0.9, R = 100, F = 0.0001, J = 0.004

$$\frac{O}{v} = \frac{0.1}{j\omega 100 * 0.004 + 0.09 + 0.01} = \frac{0.1}{j\omega 0.4 + 0.1} = \frac{1}{1 + j\omega 4}$$

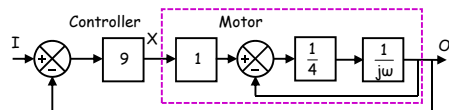


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**Connect Motor in Control System**



Use forward over 1 minus each loop

$$\frac{O}{I} = \frac{9 * \frac{1}{4} * \frac{1}{j\omega}}{1 - \frac{1}{4} * \frac{1}{j\omega} - 9 * \frac{1}{4} * \frac{1}{j\omega}} = \frac{9}{1 + \frac{1}{j\omega 4} + \frac{9}{j\omega 4}} = \frac{9}{10 + j\omega 4} = \frac{0.9}{1 + j\omega 0.4}$$

Still in standard form.

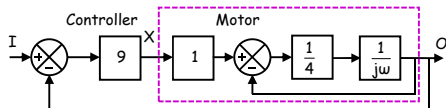
Key point : K and T of original motor changed

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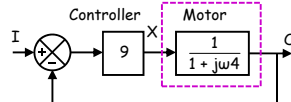


**Or Can Simplify First**



But motor is

$$\frac{1}{1 + j\omega 4}$$



$$\frac{O}{I} = \frac{9 * \frac{1}{1 + j\omega 4}}{1 + 9 * \frac{1}{1 + j\omega 4}} = \frac{9}{1 + j\omega 4 + 9} = \frac{9}{10 + j\omega 4} = \frac{0.9}{1 + j\omega 0.4}$$

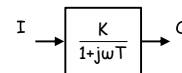
Same answer. Same form

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**Key Point to Note**



$$\left| \frac{O}{I} \right| = \frac{K}{\sqrt{1 + \omega^2 T^2}} \quad \angle \frac{O}{I} = \tan^{-1} 0 - \tan^{-1} \omega T = -\tan^{-1} \omega T$$

if I = sin(ωt)

$$O = \frac{K}{\sqrt{1 + \omega^2 T^2}} \sin(\omega t + \phi) \quad \text{where } \phi = -\tan^{-1}(\omega T)$$

Modulus of transfer function

argument of transfer function

If interested, two slides after lecture summary confirm this : Also shows that complex numbers makes it easier

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**Summary**

In this lecture we have further investigated system models  
 We assume the input is a sinusoid and model integration by  $1/j\omega$   
 For the RC circuits and the motors the same form of model found  
 When we put feedback round it, the same form of model appears

$$\frac{K}{1+j\omega T}$$

Can find output using modulus and argument of this  
 Later we develop this by considering what happens when  $\omega$  changes  
 Next week : how to model systems when inputs are not sinusoids...

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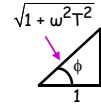


**Confirmation - if interested**

$$I = \sin(\omega t); O = \frac{K}{\sqrt{1+\omega^2 T^2}} \sin(\omega t - \phi) \text{ where } \phi = \tan^{-1}(\omega T)$$

$$\text{NB } \sin(A - B) = \sin(A) \cos(B) - \cos(A) \sin(B)$$

$$\text{So } \sin(\omega t - \phi) = \sin(\omega t) \cos(\phi) - \cos(\omega t) \sin(\phi)$$



$$\cos(\phi) = \frac{1}{\sqrt{1 + \omega^2 T^2}} \quad \sin(\phi) = \frac{\omega T}{\sqrt{1 + \omega^2 T^2}}$$

$$O = \frac{K}{\sqrt{1 + \omega^2 T^2}} \left( \sin(\omega t) \frac{1}{\sqrt{1 + \omega^2 T^2}} - \cos(\omega t) \frac{\omega T}{\sqrt{1 + \omega^2 T^2}} \right)$$

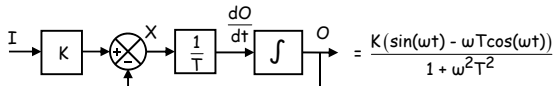
$$O = \frac{K}{1 + \omega^2 T^2} (\sin(\omega t) - \omega T \cos(\omega t))$$

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**Concluded**



$$\frac{dO}{dt} = \frac{K \cdot I - O}{T} = \frac{K \sin(\omega t) - \frac{K}{1 + \omega^2 T^2} (\sin(\omega t) - \omega T \cos(\omega t))}{T}$$

$$= \frac{K \omega^2 T^2 \sin(\omega t) + K \omega T \cos(\omega t)}{T(1 + \omega^2 T^2)} \quad \text{integrate this to get } O$$

$$O = \frac{K \omega^2 T^2 \frac{1}{\omega} \cos(\omega t) + K \omega T \frac{1}{\omega} \sin(\omega t)}{T(1 + \omega^2 T^2)} = \frac{-K \omega T \cos(\omega t) + K \sin(\omega t)}{(1 + \omega^2 T^2)}$$

*Yes - complex numbers easier*

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**Lecture 14 - Frequency Response**

We have also analysed systems where the input is a sinusoid

For this we use  $1/j\omega$  for  $\int$

As a result the transfer function is a complex number

This has modulus and argument

Which can represent gain and phase shift of system

Hence, if we know the input sinusoid we can find its output

Also useful to see how gain and phase vary with frequency

Today we plot this variation -

Using one graph, then two related graphs

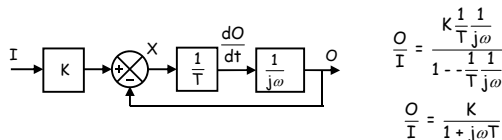
This is very useful for analysing systems

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**First Order Systems - Reminder**



$$\frac{O}{I} = \frac{K \frac{1}{T} \frac{1}{j\omega}}{1 - \frac{1}{T} \frac{1}{j\omega}}$$

$$\frac{O}{I} = \frac{K}{1 + j\omega T}$$

$$\left| \frac{O}{I} \right| = \frac{K}{\sqrt{1 + \omega^2 T^2}} \quad \angle \frac{O}{I} = \tan^{-1} 0 - \tan^{-1} \omega T = -\tan^{-1} \omega T$$

if  $I = K_1 \sin(\omega t)$

$$O = K_1 \frac{K}{\sqrt{1 + \omega^2 T^2}} \sin(\omega t + \phi) \text{ where } \phi = -\tan^{-1}(\omega T)$$

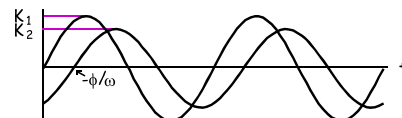
Modulus of transfer function      argument of transfer function

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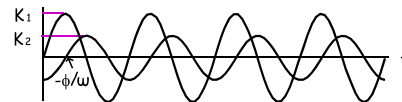
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**Input,  $K_1 \sin(\omega t)$  Output  $K_2 \sin(\omega t + \phi)$**



Higher freq : smaller  $K_2$ , larger phase shift  $-\phi$



More useful, plot graphs showing how gain and phase vary with  $\omega$

In fact we see how the transfer function varies with  $\omega$

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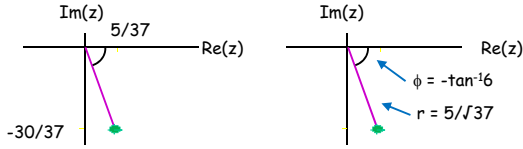


**Transfer Function at different  $\omega$**

For System  $\frac{K}{1+j\omega T}$  if  $K = 5, T = 2, \omega = 3$ , TF is  $\frac{5}{1+j6}$

$TF = \frac{5}{\sqrt{37}} \angle -\tan^{-1}6$  or  $\frac{5}{37} - j\frac{30}{37}$

Can Plot on Argand Diagram ... in Cartesian or Polar form



But if  $\omega = 1$ , System  $\frac{5}{1+j2} = \frac{5}{\sqrt{5}} \angle -\tan^{-1}2$  or  $1-j2$

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**MatLab Calculations**

`>> K = 5; T = 0.2; w = 1;`

`>> tf = K/(1+j*w*T) % find TF at w = 1`

`tf = 4.8077 - 0.9615i`

Then use `real(tf), imag(tf)` or `abs(tf), angle(tf)`

We need to make such calculations over large range ... Say 0.1 .. 1000

`>> tf = K./(1+j*[0.1, 1, 10, 100, 1000]*T) %note ./ to get TF as vector`

`tf = 4.9980 - 0.1000i 4.8077 - 0.9615i 1.0000 - 2.0000i`

`0.0125 - 0.2494i 0.0001 - 0.0250i`

`>> abs(tf) gives 4.9990 4.9029 2.2361 0.2497 0.0250`

`>> angle(tf) gives -0.0200 -0.1974 -1.1071 -1.5208 -1.5658`

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**MatLab can plot for different  $\omega$**

`>> K = 5; T = 0.2;`

`>> w = [1,2,3,4,5,6,7]; % some w`

`>> tf = K./(1+j*w*T) % calc TF at each.`

`tf =`

`4.8077 - 0.9615i 4.3103 - 1.7241i`

`3.6765 - 2.2059i 3.0488 - 2.4390i`

`2.5000 - 2.5000i 2.0492 - 2.4590i`

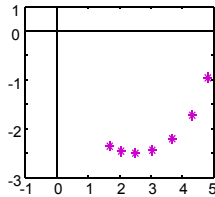
`1.6892 - 2.3649i`

`>> plot(real(tf), imag(tf), '*', [-1 5], [0 0], [0 0], [-3 1]);`

`% plot *'s and axes`

Note \*'s get closer : linearly spaced  $\omega$  not best :

So need to plot over larger  $\omega$  range .. And not linearly spaced



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**Continuous Plot in MATLAB**

Better if  $\omega$  logarithmically not linearly spaced, and join dots

Use `logspace(a, b)` : generates 50 values between  $10^a$  and  $10^b$ .

`>> w = logspace(-1,2);`

`% w from 0.1 to 100 : ok this sys`

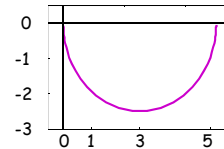
`>> tf = K./(1+j*w*T);`

`% trans func at all w`

`>> plot(real(tf), imag(tf), ...`

`% plot 'locus'`

`[-0.5,K+0.5], [0 0],[0, 0], [-K/2-0.5, 0.5]);`



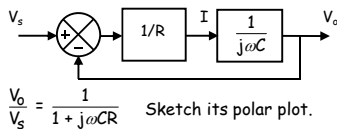
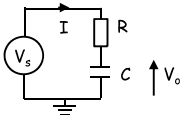
Shows how gain and phase vary with frequency on one plot - System's Frequency Response NB this is a semi-circle radius  $K/2$ , origin  $K/2, 0$

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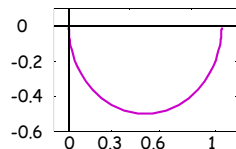


**14 - In Class Exercise**



$\frac{V_o}{V_s} = \frac{1}{1 + j\omega CR}$  Sketch its polar plot.

At very low  $\omega$ , gain is 1  
So is semi-circle  
Radius 0.5, org 0.5, 0



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**Two Plots**

The single plot shows how gain and phase vary together

Can be of interest to see how gain and phase each vary with  $\omega$

But saw polar plot calculated from  $\omega = 0$  to 100 or even 1000 rad/s

Information  $\omega = 0.1 : 1$  just as important as from 1 : 10, 10 : 100

So the  $\omega$  axis is plotted using logarithmic scales:



As gain varies a lot from 10..0.05 also use logarithmic gain scale

Phase varies from 0 to  $-90^\circ$  ... so use linear scale

So plot `log(gain) vs log(w)` and `phase vs log(w)`

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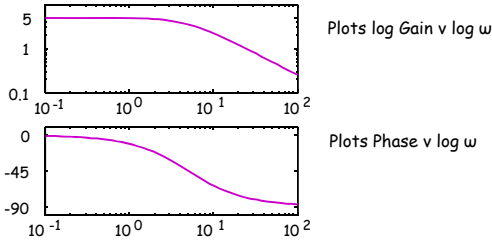
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## Bode Plot for $5/(1+j\omega 0.2)$

Given have already calculated w and tf ...

```
>> subplot(2,1,1); loglog(w,abs(tf));
>> subplot(2,1,2); semilogx(w, angle(tf)*180/pi);
```



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## Approximate Behaviour

Recall:  $TF = \frac{K}{1+j\omega T}$  ; Gain =  $\frac{K}{\sqrt{1+\omega^2 T^2}}$  ; Phase =  $-\tan^{-1}(\omega T)$

Suppose  $\omega T$  very small ( $\ll 1$ ), so treat  $1 + j\omega T$  as 1

$TF = \frac{K}{1}$ , so Gain = K; Phase = 0

Suppose  $\omega T$  very big ( $\gg 1$ ), so approximate  $1 + j\omega T$  as  $j\omega T$

$TF = \frac{K}{j\omega T}$ , so Gain =  $\frac{K}{\omega T}$ ; Phase =  $-90^\circ$

These define behaviour at very low and very high freq

Actual behaviour in between these, eg

At  $\omega T = 1$   $TF = \frac{K}{1+j}$  ; Gain =  $\frac{K}{\sqrt{1+1}} = \frac{K}{\sqrt{2}}$  ; Phase =  $-45^\circ$

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## Plotting Approximate Behaviour

At Low Freqs, approximate Gain = K and Phase = 0

Plot  $\log(\text{Gain})$  vs  $\log(\omega)$   $\log(K)$  is constant

So Plot horizontal straight line : its slope is 0

At High Freqs, Gain =  $\frac{K}{\omega T}$  and Phase =  $-90^\circ$

$\log\left(\frac{K}{\omega T}\right) = \log\left(\frac{K}{T} * \omega^{-1}\right) = \log\left(\frac{K}{T}\right) + \log(\omega^{-1}) = \log\left(\frac{K}{T}\right) - \log(\omega)$

So Plot is const -  $\log(\omega)$  plotted vs  $\log(\omega)$

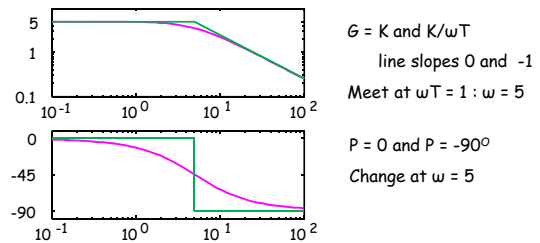
Like plotting  $c - x$  vs  $x$  ie straight line slope -1

We call these high and low freq lines asymptotes

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## Asymptotic Plot (actual superimposed)

Asymptotic TF : K and  $\frac{K}{j\omega T}$  ie 5 and  $\frac{5}{j\omega 0.2} = \frac{25}{j\omega}$



$G = K$  and  $K/\omega T$

line slopes 0 and -1

Meet at  $\omega T = 1$  :  $\omega = 5$

$P = 0$  and  $P = -90^\circ$

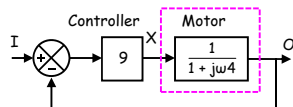
Change at  $\omega = 5$

Actual plots start on low freq asymptotes and end on high f lines

Given TF, easy to sketch asymptotes and then add actual

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## Freq Response of Motor in Feedback



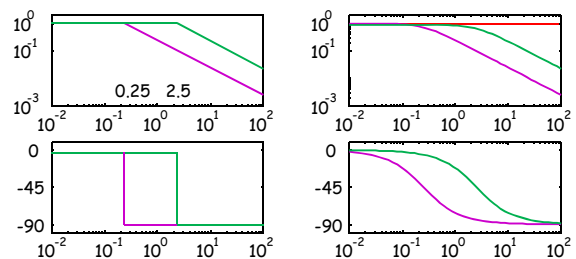
$$\frac{O}{I} = \frac{9 * \frac{1}{1+j\omega 4}}{1 + 9 * \frac{1}{1+j\omega 4}} = \frac{9}{1+j\omega 4 + 9} = \frac{9}{10+j\omega 4} = \frac{0.9}{1+j\omega 0.4}$$

With feedback, corner freq moved from 0.25 to 2.5 rad/s

Let's plot superimposed  $\frac{1}{1+j\omega 4}$  and  $\frac{0.9}{1+j\omega 0.4}$

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## Graphs ... Asymptotes and actual

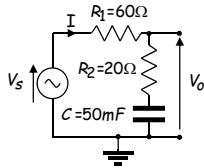


With feedback, Gain higher over more frequencies

Phase near 0 over more frequencies

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**Phase Lag System**



Treat like Potential Divider ...  
 $(V_s - V_o) / R_1$  determines current  
 Current through  $R_2 + C$  sets  $V_o$   
 $R_2 + \frac{1}{j\omega C} = \frac{j\omega CR_2 + 1}{j\omega C} = \frac{j\omega + 1}{j\omega 0.05}$

$$V_o = \frac{1}{1 + \frac{1}{60} \cdot \frac{j\omega + 1}{j\omega 0.05}} = \frac{60 \cdot j\omega 0.05}{j\omega 3 + j\omega + 1} = \frac{j\omega + 1}{j\omega 4 + 1}$$

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**Continued**

$$\frac{V_o}{V_s} = \frac{j\omega + 1}{j\omega 4 + 1} \quad \text{Two corner freqs : } \frac{1}{4} \text{ and } 1 \text{ rad/s}$$

We can plot this by generating asymptotes as before  
 For each  $1+j\omega T$ , approx as 1 before  $\omega = 1/T$ , and  $j\omega T$  after  
 So consider what happens before  $\frac{1}{4}$ , from  $\frac{1}{4}$  to 1, then after 1

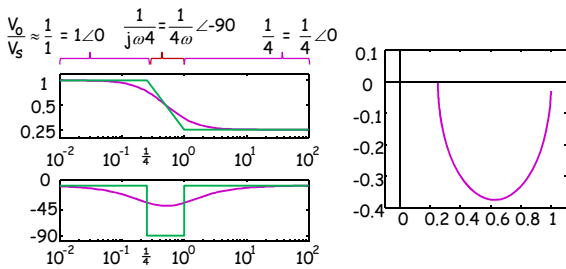
So $\omega < 0.25$	$0.25 < \omega < 1$	$\omega > 1$
$\frac{V_o}{V_s} \approx \frac{1}{1} = 1$	$\frac{V_o}{V_s} \approx \frac{1}{j\omega 4}$	$\frac{V_o}{V_s} \approx \frac{j\omega}{j\omega 4} = \frac{1}{4}$
Gain = 1	Gain = $\frac{1}{\omega 4}$	Gain = 0.25
Phase = 0	Phase = -90	Phase = 0

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**Bode and Polar Plots**



In mid freqs, around  $\sqrt{1 \cdot 4} = 0.5$  rad/s, phase is -ve, so  $V_o$  'lags'  $V_s$   
 Such a 'phase lag' circuit can be used for control

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**Summary**

In this lecture we consider plotting frequency response  
 That is, how does system transfer function vary with  $\omega$ .  
 We first plotted these on one graph  
 Calculating gain/phase or real + j imag points and joining them  
 Then we plotted log(gain) vs log( $\omega$ ) and phase vs log( $\omega$ )  
 Both the actual graphs and the asymptotes  
 Asymptotes useful for sketching such graphs  
 Saw that with phase lead circuit.  
 Next week we move to considering how system changes with time  
 We will do frequency response of second order systems later

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**15 - Time Response of Systems**

We modelled different dynamic systems which include integrators  
 We have determined their output

- If the input is a step, the output is a constant value
  - determined by when the input to the integrator is 0
- If the input is a sinusoid, the output is also a sinusoid
  - determined by modelling the system using complex numbers

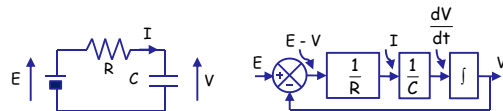
This answered one of two questions posed  
 The other is how does the output get to its final value.  
 Strictly so far we have determined the steady state response  
 We now work towards how it gets there: the transient response

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**Consider the RC Circuit**



$$\text{From block diagram, } \frac{dV}{dt} = I \cdot \frac{1}{C} = (E - V) \cdot \frac{1}{R} \cdot \frac{1}{C}$$

When E is connected at  $t = 0$ , in effect it is a step input  
 V will reach the final value of E (which is constant after  $t=0$ )  
 Final value means V not changing, ie  $dV/dt = 0$   
 Clearly this is when  $I = 0$ , which is when  $E - V = 0$ , or  $V = E$

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### Now consider a motor and general system

From block diagram,  
 $\frac{dO}{dt} = \frac{1}{m}(v*k - F*O)$

If  $v$  is step applied at  $t = 0$   
 Oss when  $v * k - F * O = 0$ ,  
 or  $O = v * k / F$

$\frac{dO}{dt} = \frac{1}{T}X = \frac{I*K - O}{T}$

$I*K - O_{ss} = 0$  or  $O_{ss} = I*K$

We argue intuitively how  $O$  or  $V$  gets to steady state .. Use integrators

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### If Put Constant Into An Integrator:

If  $O$  is  $\int$  block output  
 $\frac{dO}{dt}$  must be block input

Or, if  $K$  smaller, and  $O$  is not 0 initially

At time  $t$ ,  $O = (\text{value of } O \text{ at } t = 0) + K * I * t$

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### What if I series of constants?

Suppose  $K = 2$  and at  $t = 0$ ,  $O = 0$ ,

- $I = 1$  from 0..5s,
- $I = -0.5$  from 5..8s,
- and  $I$  thereafter = 0.25

After 5s,  
 $O = 0 + 1*2*5 = 10$

After 8s,  
 $O = 10 + -0.5*2*3 = 7$

After 10s,  
 $O = 7 + 0.25*2*2 = 8$

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### If Put Feedback Round Integrator

$O = 0$  at  $t=0$ ;  
 $I$  is 1

Initially  $O$  is 0, so  $X$  &  $dO/dt$  are big, so  $O$  rises much  
 $X$  and  $dO/dt$  now smaller, so  $O$  rises but by less  
 $X$  and  $dO/dt$  even smaller, so  $O$  rises by even less  
 Eventually  $O = I$ , so  $X = dO/dt = 0$ , and hence  $O$  is constant

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### Step Responses

Often we analyse systems as follows:

- At time  $t = 0$ , output  $O = 0$ , input turned on
- $I$  goes 0 to value: is a 'step' (unit step if value = 1)
- $O$  moves smoothly from 0 to a final value
- Called an exponential lag (it lags behind input)

$O$  reaches a (constant) value - its steady state;  
 How gets there is the (exponential) transient response

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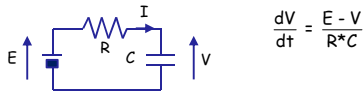
### Formalising The Response

$X = I * K - O$   
 So  $\frac{dO}{dt} = \frac{1}{T}(K*I - O)$

At steady state,  $dO/dt = 0$ , that is  $K*I - O = 0$   
 So steady state value of  $O$  is  $K * I = K$  if  $I$  is unit step  
 In Maths, you will learn to show transient response is  $-Ke^{-t/T}$   
 Done by solving  $\frac{dO}{dt} = -\frac{O}{T}$  (i.e. ignoring input  $I$ )  
 The complete response is  $O = K - Ke^{-t/T}$

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**So for RC circuit**



Steady state found by solving  $\frac{dV}{dt} = 0$  So  $V_{ss} = E$

Transient found by solving  $\frac{dV}{dt} = -\frac{V}{R * C}$  So  $V_t = -E e^{-t/RC}$

So complete response is  $V = E - E e^{-t/RC}$

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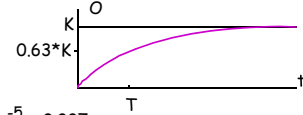
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**Fundamental Point**

If system model  $\frac{dO}{dt} = \frac{1}{T}(K * I - O)$ ; I = unit step; O at t= 0 is 0

Then  $O = K - K e^{-t/T}$



$e^{-1} \approx 0.37$ ;  $e^{-3} \approx 0.05$ ;  $e^{-5} \approx 0.007$

At  $t = T$ ,  $K - K e^{-1} = K * 0.63$  (O is 63% of final value)

At  $t = 3T$ ,  $K - K e^{-3} = K * 0.950$  (O is 5% from final value)

At  $t = 5T$ ,  $K - K e^{-5} = K * 0.993$  (O <1% from final value)

<http://www.reading.ac.uk/~shsmchr/javascrip/SysAndStep.html>

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**If you are interested ...**

We have stated that I is a unit step, = constant for  $t > 0$

$$O(t) = K - K * e^{-t/T}$$

$$\text{Also } \frac{dO}{dt} = \frac{1}{T}(K * I - O)$$

This demonstrates that these are consistent

$$\frac{dO}{dt} = \frac{dK}{dt} - \frac{d(K * e^{-t/T})}{dt} = 0 - \frac{1}{T} K * e^{-t/T} = \frac{K}{T} e^{-t/T}$$

$$\frac{1}{T}(K * I - O) = \frac{1}{T}(K - K + K * e^{-t/T}) = \frac{K}{T} e^{-t/T}$$

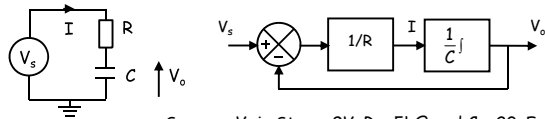
Hence expression for O is a solution to the diff eqn

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**Electronic Example**



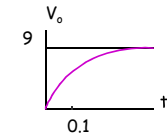
Suppose  $V_s$  is Step = 9V;  $R = 5k\Omega$  and  $C = 20\mu F$

$$\frac{dV_o}{dt} = \frac{1}{5 * 10^3 * 20 * 10^{-6}} * (9 - V_o)$$

$$\frac{dV_o}{dt} = \frac{1}{0.1} * (9 - V_o)$$

In standard form, so if  $V_o = 0$  at  $t=0$

$$V_o = 9 - 9 e^{-t/0.1}$$

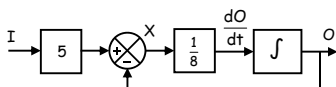


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**Lecture 15 - In Class Exercise**



Derive an expression for  $dO/dt$  in standard form.

Suppose I = step height 1 applied at  $t = 0$  when  $O = 0$ :

Sketch a graph of O versus t : label final value and time constant.

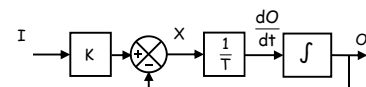
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**Effect of Feedback - to Step Input**

System could be motor on its own: open loop

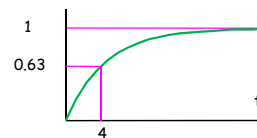


$$\text{Modelled by } \frac{dO}{dt} = \frac{K * I - O}{T}$$

Suppose  $I = 1$ ,  $K = 1$  and  $T = 4s$   $\frac{dO}{dt} = \frac{1 * 1 - O}{4} = \frac{1 - O}{4}$

In standard form, so can say:

- Steady State value 1
- Reaches 63% of 1 at 4s
- Within 1% of 1 by 20s

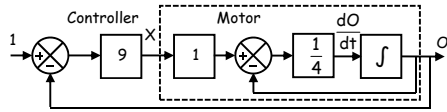


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**Now This Motor In Control System**



Controller output =  $9*(1-O)$ ,  $X = 9*(1-O) - O$ , so

$$\frac{dO}{dt} = \frac{1}{4} * (9*(1 - O) - O) = \frac{9 - 9*O - O}{4} = \frac{9 - 10*O}{4}$$

Not in right form as O multiplied by 10: so divide by 10

$$\frac{dO}{dt} = \frac{9/10 - O}{4/10} = \frac{0.9 - O}{0.4} \quad \text{Final value } 0.9. \text{ Reach } 63\% \text{ of this at } t = 0.4s$$

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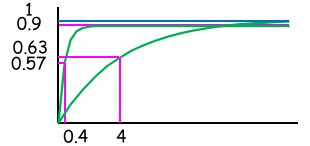
**Open and Closed Loop Responses**

Open loop:  $\frac{dO}{dt} = \frac{1-O}{4}$

Final value 1  
Time Const 4

Closed loop:  $\frac{dO}{dt} = \frac{0.9-O}{0.4}$

Final value 0.9  
Time Const 0.4



See Frequency Response Lectures: same example: same 0.9 & 0.4

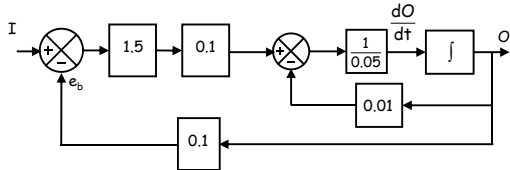
<http://www.reading.ac.uk/~shsmchr/javascript/SysAndStep.html>

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**Another Example - Motor**



$$\frac{dO}{dt} = \frac{1}{0.05} ((I - 0.1*O)*0.15 - 0.01*O)$$

$$\frac{dO}{dt} = \frac{1}{0.05} (I*0.15 - 0.025*O)$$

Now in standard form,  $K = 0.6, T = 2$  so if I step

$$\frac{dO}{dt} = \frac{1}{2} (I*0.6 - O)$$

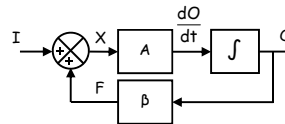
$$O(t) = 0.6 - 0.6 * e^{-t/2}$$

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**Aβ Feedback System With Integrator**



$$\frac{dO}{dt} = A(I + \beta O)$$

For standard form, re jigs so  $\frac{dO}{dt} = \frac{1}{T}(K*I - O)$

$$\frac{dO}{dt} = -A(I - \beta O) = -A\beta(-\frac{I}{\beta} - O)$$

So  $K = -1/\beta$  and  $T = -1/A\beta$ ;

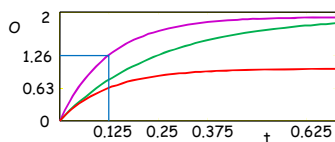
Feedback gain  $\beta$  sets final value, loop gain  $A\beta$  the speed

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**Some Example Responses**



I = 1  
a)  $A = 16, \beta = -0.5$   
b)  $A = 8, \beta = -0.5$   
c)  $A = 8, \beta = -1$   
Want final value & t when 63% of it

	A	β	Final Value	t at 63%	I/-β	1/-Aβ
a	16	-0.5	2	0.125	2	1/8
b	8	-0.5	2	0.25	2	1/4
c	8	-1	1	0.125	1	1/8

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**Summary**

We have investigated the step response of a first order system

Have seen steady state response - being a constant

And transient response - being an exponential

The time constant indicates the speed of response :

reaches 63% of final value at  $t =$  time constant

within 1% of final value at  $5 * \text{this value}$

We have seen that putting feedback round such systems, speeds up the response

Next week, we introduce the s-operator

to simplify diagrams/analysis .. Be consistent with jw

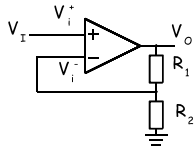
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Lecture 11 - After Class Exercise



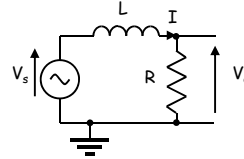
Find  $V_o$  if  $V_i = 1V$ , OpAmp gain  $A = 1000$ ,  $R_1 = 80k\Omega$  and  $R_2 = 20k\Omega$ .  
 Note, find the exact value, and compare with the approximate one.  
 By how much does  $V_o$  change, if  $A$  increases by 10% to 1100?  
 Does the system have negative feedback?

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Lecture 12 - After Class Exercise



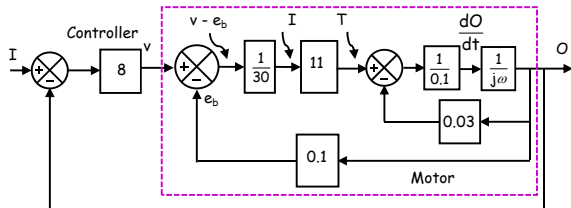
If  $V_L$  is the voltage across the inductor,  $I = V_L/j\omega L$ .  
 As such, draw a block diagram of the circuit.  
 Hence work out the circuit transfer function.  
 What is  $V_o$  if  $L = 0.5H$ ,  $R = 20\Omega$  and  $V_s$  is  $7 \sin(8t)$ ?

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Lecture 13 - After Class Exercise



The above shows a permanent magnet motor in a control system  
 Use forward / (1 - loops) to find the transfer function  $O/I$ .  
 What is  $O$  if  $I$  is  $9 \sin(40 t)$ ?

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